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AMENDMENTS TO THE SPECIFICATION

Please replace the paragraph beginning at page 3, line 2, and ending at line 17 with

the following amended paragraph:

In such sheet discharging apparatus, when the sheet is discharged at a high speed to the

endless belt by the discharging means, the rear edge of the sheet is nipped by a roller pair for

conveying the sheet in the plural rows, and there is a difference between the conveying speed of

the roller pair and the discharging speed of the discharging means. Accordingly, in order to

discharge at high speed to the endless belt, it is necessary to eliminate for the difference. In the

above publications No. 3286598 and 2812143, the sheet discharging apparatus is provided with a

one-way clutch between a conveyer roller of the roller pair disposed along the plural rows and a

shaft for coaxially supporting the conveyer rollers. When the discharging at the high speed to the

endless belt is performed, the one-way clutch effects operates to release the conveyer roller from

the driving system. Thus the conveyer roller freely rotates such that the sheet may smoothly

leave the roller pair.

Please replace the paragraph beginning at page 3, line 18, and ending at line 31 with

the following amended paragraph:

However, in order to eliminate for the difference between the conveying speed of the

conveying roller and the discharging speed by the discharging means in this structure of free

rotation of the conveying roller $\frac{d}{dt} = \frac{dt}{dt} = \frac{dt}{dt} = \frac{dt}{dt}$ large number of the

one-way elutch-clutches is provided in accordance with the length variation of the cut sheet to be

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used in the above sheet discharging apparatus. As the one-way clutch is expensive, the a low cost

for production is difficult. Further, as the one-way clutch is attached to one roller of the conveyer

roller pair, the roller nip force of the another other roller of the conveyer roller pair is applied as

the a bending moment and the an excess radial load to the one-way clutch and the conveyer

roller, and therefore breaks the one-way clutch. Therefore, the durability of such a clutch is not

so high.

Please replace the paragraph beginning at page 4, line 1, and ending at line 23 with

the following amended paragraph:

In the publication No. 2765652, a torque limiter is provided between a drive shaft and a

drive roller of a high speed discharging means. The torque limiter has effects operates to freely

rotate the drive roller, when a torque applied to the drive roller is at least a predetermined value.

Thus the difference between the conveying speed of the conveyer roller and the discharging

speed of the drive roller of the discharging means is eliminated. The drive roller is supported by

a frame attached to the drive shaft. There is also a gear drive transmission mechanism between

the drive roller and the drive shaft. Thus the drive force of the drive shaft is transmitted through

the gear drive transmission mechanism and the torque limiter to the drive roller. Accordingly, the

structure around the drive roller is complicated, the cost is high, and it is hard to keep the area for

deposition of the parts. Further, the torque limiter is the so-called magnet-magnetic particle type,

and therefore expensive, which make the cost higher. Furthermore, in the publication No. No. 60-

23343, a clutch mechanism which is constructed of a solenoid and a pair of clutch plates is used

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instead of the one-way clutch and the torque limiter. In this case, however, the number of the

parts becomes larger, and many controlling means are necessary, which prevents the-decrease of

the cost.

Please replace the paragraph beginning at page 5, line 3, and ending at line 18 with

the following amended paragraph:

In order to achieve the object and the other object, a sheet discharging apparatus of the

present invention has a conveying means for conveying a sheet on a conveying path and a high

speed discharging means for discharging out the sheet at high speed. The high speed discharging

means is positioned near the exit, and a discharging speed is higher than a conveying speed of

the conveying means. The high speed discharging means comprises a drive roller, a nip roller

and a frictional connection unit. The drive roller is rotatably and coaxially attached to a drive

shaft, and is unshiftable in an axial direction of the drive shaft. The nip roller contacts to the

drive roller, and rotates in accordance with rotation of the drive roller to nip the sheet with the

drive roller. The frictional connection unit has a-the function of a friction clutch, and firmly

eombines couples the drive roller and the drive shaft with by friction.

Please replace the paragraph bridging pages 5 and 6 with the following amended

paragraph:

In a preferable preferred embodiment of the present invention, the friction member is

provided with a contact portion for contacting the drive roller. The contact portion is chamfered

to have an arc-shape or a linear inclination or arc-shape to an axial direction of the drive roller.

The sheet is conveyed on said path in a situation that the sheets are positioned in zigzag in plural rows, and sequentially arranged in a single row after discharged by the discharging apparatus.

Please replace the paragraph beginning at page 8, line 14, and ending at line 17 with the following amended paragraph:

As shown in FIGs.FIGs. 2A-2C, the sheet dispenser 10 dispenses the sheets 15-17 into one or plural FOW-rows in accordance with the sheet size. In this situation, each sheet 15-17 is sent to the development device 18 and the dryer 19.

Please replace the paragraph beginning at page 9, line 4, and ending at line 6 with the following amended paragraph:

As shown in FIG. 2C, the large size sheet 17 is not dispensed but deposited and conveyed in one row on all-over the first-third conveying paths 21-23.

Please replace the paragraph beginning at page 12, line 15, and ending at line 23 with the following amended paragraph:

The high speed discharging roller pair 50 disposed near the exit 47 of the primary path 44 is constructed of a drive roller 63 and a nip roller 64. As shown in FIG. 5, the plural drive rollers 63 are rotatably and coaxially attached to a metallic shaft 65 with the same intervals between the neighboring drive rollers 63. It is to be noted in this figure that the number of the drive rollers 63 on the shaft 65 is six. There is a frictional connection unit (friction clutch) 66 between the cach drive roller 63 and the shaft 65.

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Please replace the paragraph beginning at page 13, line 13, and ending at line 20

with the following amended paragraph:

The drive roller 63 is a roller produced from synthesized polymer, and the surface of the

drive roller 63 is coated with a rubber coating 72. As the synthesized polymer, there are materials

which is are excellent in slip properties, abrasion resistance. Such materials are, for example,

polyacetal (POM), polyamide (PA), ultra-high-molecular polyethylene (PE-UHMW),

polyethylene sulfide (PPS), polytetrafluoroethylene (PTFE) and the like.

Please replace the paragraph bridging pages 13 and 14 with the following amended

paragraph:

The friction member 74 is nearly-cylindrically shaped, and coaxially attached to the shaft

65 so as to be slidable in the axial direction. The friction member or pad 74 has a compression

contact surface 74a which contacts to the side surface 63b of the drive roller 63. In the middle of

the contact surface 74a, a notch 74b is formed. Further, in an opposite side to the contact surface

74a, the friction member 74 has a recess 74c continuing to a through hole 74e through which the

shaft 65 is inserted. Note that the friction member 74 is formed from the same synthesized

polymer as the drive roller 63. The notch 74b is formed so as to have the a diameter for fitting to

the E-ring 71b.

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Please replace the paragraph beginning at page 14, line 22, and ending at line 27

with the following amended paragraph:

When a force of more than a predetermined value is applied to the drive roller to rotate in

a direction B (see, FIG.7), there occurs a slide-slippage between the drive roller 63 and the

friction member 74 against the bias of the coil spring 75. Accordingly, the drive roller 63 rotates

at the-a smaller rotational speed than the shaft 65.

Please replace the paragraph bridging pages 20 and 21 with the following amended

paragraph:

As shown in FIG. 8A, the sheet 16 is conveyed with the conveying roller pair 49 at the

conveying speed VA in accordance with the rotation of the conveying roller pair 49. In the high

speed discharging roller pair 50, it is to be noted that the shaft 65 and the drive roller 63 are

firmly eombined with coupled by friction by via the frictional connection unit 66, so as to rotate

together. The discharging speed of the high speed discharging roller pair 50 is $V_{\rm B}$ (>V_A). The

sheet 16 conveyed to the high speed discharging roller pair 50 is nipped with the drive roller 63

and the nip roller 64. As shown in FIG. 8B, a front edge 16a of the sheet 16 is nipped with the

high speed discharging roller pair 50. Thereby as a rear edge 16b of the conveying roller pair 49

sheet 16 is nipped, the sheet 16 is tensed toward the rear edge 16b at a tension force which is

larger than the a predetermined value. Accordingly, the tension force is transmitted to the drive

roller 63 so as to rotate in the direction opposite to the rotational direction. Thus the drive roller

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63 slips on the frictional connection unit 66. Accordingly, the drive roller 63 rotates at the lower rotational speed V_B, than the rotational speed V_B, (V_B'< V_B), and the difference between the conveying speed of the conveying roller pair 49 and the discharging speed of the high speed

discharging roller pair 50 is eliminated to discharge the sheet 16 sequentially.

Please replace the paragraph beginning at page 22, line 5, and ending at line 31 with the following amended paragraph:

Further, the frictional connection unit 66 is provided coaxially with the drive roller 63 and the shaft 65, and has a simple structure for transmitting the drive force. The number of parts of the frictional connection unit 66 is small, and therefore the cost for producing the frictional connection unit 66 is low. Furthermore, the drive roller 63 and the friction member 74 are formed of the synthetic polymer, polymers, and the load by the slips-slippage between the two members can be easily calculated from the biasing force, applied by the biasing means applied with—a biasing member, and the frictional coefficient—coefficients of the—both synthetic polymerpolymers. Further, while the bias pressure is calculated from the contact area of the synthetic polymer and the biasing force applied by the biasing member, the upper limit of abrasion in slip can be estimated from the multiple (PV value) of the averaged speed and the bias pressure. Thus when the—a predetermined load is applied, the frictional connection unit 66 is effective to discharge the sheet sequentially. If the—a torque limiter of the magnetic sand type is used instead of the frictional connection unit 66, then the cost for production becomes higher. Further, the torque limiter slips when the sheet is discharged. In this case, the-high endurance is

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necessary. Furthermore, when the endurance is near the limit thereof, the load of the slip varies so much. Therefore the sheet 16 cannot be discharged sequentially. Further, since there is a difference of in the limit-limits of the-endurance between products-components of the torque limiter, it becomes extremely difficult to maintain the-stability of the discharging.

Please replace the paragraph beginning at page 23, line 6, and ending at line 28 with the following amended paragraph:

Note that the shape and the form of the drive roller and the frictional connection unit that construct form the high speed discharging roller pair is are not limited in to the above embodiment. For another embodiment, see FIGs-FIGs, 9 and 10. In FIGs, 9, 10 the same members and parts has have the same numerals as the above embodiment, and the explanations thereof are omitted. In a frictional connection unit 128 illustrated in FIG. 9, a tip 129a of the friction member or pad 129 has a taper surface 129b. The taper surface 129b is formed to have a constant inclination to an axis of the drive roller 130. Further, one side 130a of the drive roller 130 has a recess 130b so as to accept the top of the tapered portion of the friction member 129. The diameter of the recess 130b is smaller than the outer diameter of the taper surface 129b. As the frictional connection unit 128 and the drive roller 130 have such structure, the friction member 129 biased by the coil spring 75 presses the outer edge of the recess 130b. Accordingly, the friction member 129 and the drive roller 130 are more effectively combined coupled with the friction by the larger pressure. When the larger load of the rotation is applied, the slip occurs between the friction member 129 and the drive roller 130. The embodiment of FIG. 9 is adequate for the case when the specifically large load of the rotation is applied.

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Please replace the paragraph bridging pages 24 and 25 with the following amended

paragraph:

In the above embodiment, the photosensitive material drawn from the magazine is cut by

the cutter 7 to have a predetermined size. The position of the cutter 7 may be upstream from the

sheet dispenser 10, and is not restricted in the above embodiment. Further, the cutting direction

of the cutter 7 is a widthwise direction of the photosensitive material, and the print size of the cut

sheet depends on the length of convey before cutting. Further, in the above embodiment, the

width of the print size in the widthwise direction is changed by selecting one of the plural

photosensitive material materials which have different width widths. However, a slitter may be

provided so as to cut the photosensitive material in the conveying direction, and to change the

width of the cut recording material. The number of the-used magazine-magazines is not restricted

in-to two, but may be equal to or more than three.